

**ChE 548**  
**Advanced Transport Phenomena II**  
**Final Exam**  
**Friday, May 1, 2009**  
**8:00-10:00 AM**

**Problem 1. Mass Transfer**

Consider diffusion of through a reactive membrane of component A, which can react to form B via the first order, irreversible reaction,  $A \rightarrow B$ . The rate constant is given by

$$k = k_o \exp\left(-\frac{E_a}{RT}\right) \quad (1.a)$$

where the rate of reaction is given by

$$rate = k\rho_A \quad (1.b)$$

The heat of reaction for this reaction is small and the system can be assumed to be isothermal.

The prefactor is  $k_o = 1.0 \times 10^{-2} \frac{1}{s}$ , the activation energy is  $E_a = 1.0 \times 10^4 \frac{J}{mol}$ ,  $R$  is the ideal gas

constant,  $R = 8.314 \frac{J}{mol \cdot K}$ , and the temperature is  $T = 300 K$ . There is no convection in the

membrane. The Fickian diffusivity is  $D = 1.0 \times 10^{-5} \frac{m^2}{s}$  and can be considered independent of

composition. The membrane is of thickness  $L = 0.05 m$ . One of boundaries of the membrane is

fixed at  $\rho_A = 0.7 \frac{kg}{m^3}$  and  $\rho_B = 0.0 \frac{kg}{m^3}$ .

(a) Write the transient total mass balance and mass of A balance.

(b) Determine the mass fraction of component A at the far side of the membrane at steady state.

(c) If you want the conversion to be 90%, how thick would the membrane have to be?

**Problem 2. Reference States in Energy Balances**

The enthalpy of component i can be written as

$$H_i(T, p) = \int_{T_{ref}}^T C_{p,i}(T, p) dT + \int_{p_{ref}}^p \left( \frac{\partial H_i}{\partial p} \right)_{T=T_{ref}} dp + H_{f,i}(T_{ref}, p_{ref}) \quad (1)$$

where  $H_{f,i}$  is the enthalpy of formation at the reference state. Typically we ignore the pressure dependence of the enthalpy. It can be ignored in this problem as well.

Consider a system with accumulation, convection and diffusion of a binary mixture, in which the mixture enthalpy is ideal

$$H_{mix}(T, p) = w_A H_A(T, p) + w_B H_B(T, p) \quad (2)$$

The total conduction in the system is due to thermal conduction and enthalpy carried by diffusion,

$$\mathbf{q} = -k_c \nabla \cdot \mathbf{T} + H_A \mathbf{j}_A + H_B \mathbf{j}_B \quad (3)$$

(a) If the system is non-reactive, show that the enthalpy of formation drops out of the energy balance.

(b) If there is a chemical reaction term, show that the enthalpy of formations terms in the energy balance become the heat of reaction term.

### Problem 3. Adsorption

Consider a system where an ideal gas adsorbs onto a surface via the Langmuir adsorption isotherm.

$$\theta_i = \frac{K_i c_i}{1 + \sum_{j=1}^{N_c} K_j c_j} \quad (1)$$

where  $c_i$  is the molar concentration of component  $i$  (mole/m<sup>3</sup>),  $\theta_i$  is the fractional occupancy of the surface, and  $K_i$  is the adsorption/desorption equilibrium coefficient with units of m<sup>3</sup>/mole.

The equilibrium coefficient is given in terms of the entropy and enthalpy of adsorption as

$$K_i = k_{o,i} \exp\left(\frac{\Delta S_i}{R}\right) \exp\left(-\frac{\Delta H_i}{RT}\right) \quad (2)$$

(a) As the temperature increases, what happens to the amount of material adsorbed? Why?

(b) As the pressure increases, what happens to the amount of material adsorbed? Why?

(c) For a binary system, will the selectivity,  $s$ , (defined below), will the selectivity increase or decrease with temperature? Why?

$$s = \frac{x_{ads,B} / x_{bulk,B}}{x_{ads,A} / x_{bulk,A}} \quad (3)$$

*Possibly Useful Information:*

The solution to an ODE of the form,  $\frac{\partial^2 y(x)}{\partial x^2} = ky(x)$ , is  $y(x) = c \exp(-\sqrt{k}x)$ .

### Balance Equations

total mass:

$$\frac{\partial \rho}{\partial t} = -\nabla \cdot (\rho \mathbf{v}) \quad , \quad (1)$$

where  $\rho$  is the mass density,  $\mathbf{v}$  is the center-of-mass velocity, and  $t$  is time.

mass balance on component A

$$\rho \frac{\partial w_A}{\partial t} = -\rho \mathbf{v} \cdot \nabla w_A - \nabla \cdot \mathbf{j}_A + \sum_{i=1}^{N_R} r_{i,A} \quad , \quad (2)$$

where  $w_A$  is the mass fraction of component A,  $\mathbf{j}_A$  is the diffusive mass flux of component A relative to the center-of-mass velocity,  $N_R$  is the number of independent chemical reactions in the system, and  $r_{i,A}$  is the rate of production of component A in reaction  $i$ , in units of mass/volume/time.

momentum balance:

$$\rho \frac{\partial \mathbf{v}}{\partial t} = -\rho \mathbf{v} \cdot \nabla (\mathbf{v}) - \nabla p - \nabla \cdot \boldsymbol{\tau} - \rho \nabla \hat{\Phi} \quad , \quad (3)$$

where  $p$  is the pressure,  $\boldsymbol{\tau}$  is the extra stress tensor, and  $\hat{\Phi}$  is the specific external field imposed by, for example, gravity. If gravity is the source of the external field then we have  $\mathbf{g} = -\nabla \hat{\Phi}$

energy balance

$$\frac{\partial \rho \left( \frac{1}{2} v^2 + \hat{H} + \hat{\Phi} \right)}{\partial t} - \frac{\partial p}{\partial t} = -\nabla \cdot \rho \left( \frac{1}{2} v^2 \cdot \mathbf{v} + \hat{H} \mathbf{v} + \hat{\Phi} \mathbf{v} \right) - \nabla \cdot \mathbf{q} - \nabla \cdot (\boldsymbol{\tau} \cdot \mathbf{v}) \quad (4)$$

where  $\hat{H}$  is the specific (per mass) enthalpy,  $\hat{\Phi}$  is the specific potential energy due to an external field, and  $\mathbf{q}$  is the heat flux due to conduction.