#### CBE 450 Chemical Reactor Fundamentals Fall, 2009 Homework Assignment #6 Solutions

#### 1. Reactors in Series

Consider the reaction

$$A + B \rightarrow C$$

with elementary mechanism such that the rate is

$$r = kC_A C_B$$

where the rate constants are given by

$$k = k_o \exp\left(-\frac{E_a}{RT}\right)$$

The temperature is 300 K. The activation energy for the reaction is 5000 J/mol. The rate constant prefactor for the reaction is 0.001 liter/mol/s. The feed flowrate is 2 liters/sec. The concentration of A in the feed stream is 10 mol/liter. The concentration of B in the feed stream is 15 mol/liter. The concentration of C in the feed stream is 0 mol/liter. Consider a CSTR of 100 liters and a PFR of 100 liters total volume.

(a) What is the net conversion of A if the reactors are placed in series with the CSTR first and PFR second?

(b) What is the net conversion of A if the reactors are placed in series with the PFR first and CSTR second?

# Solution:

(a) What is the net conversion of A if the reactors are placed in series with the CSTR first and PFR second?

We analyze the CSTR first.

The input file is

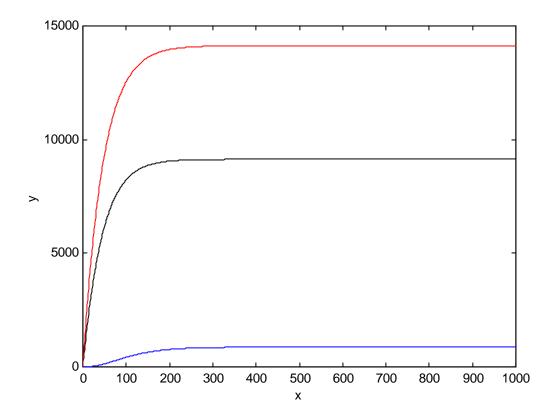
```
function dydt = sysodeinput(x,y,nvec);
%
% one reaction
% A + B --> C
%
% example usage:
% [y,x] = sysode(2,1000,0,1000,[0,0,0]);
%
```

CA = y(1);CB = y(2);CC = y(3);% nuA = -1.0;nuB = -1.0;nuC = 1.0;% % constant volume; F = 2.0; % liter/sec F = 2.0/1000; % m^3/sec Fin = F;Fout = F; CAin = 10.0; % mol/liter CBin = 15.0; % mol/liter CCin = 0.0; % mol/literCAin = CAin\*1000; % mol/m^3 CBin = CBin\*1000; % mol/m^3 CCin = CCin\*1000; % mol/m^3 % V = 100; % liter V = 100/1000; % m^3 R = 8.314; % J/mol/K T = 300; % K ko = 1.0e-3; % liter/mol/sec ko = ko/1000; % m^3/mol/sec Ea = 5000; % J/mol k = ko\*exp(-Ea/(R\*T));rate = k\*CA\*CB; % % molar balances % dydt(1) = Fin/V\*CAin - Fout/V\*CA + nuA\*rate; dydt(2) = Fin/V\*CBin - Fout/V\*CB + nuB\*rate; dydt(3) = Fin/V\*CCin - Fout/V\*CC + nuC\*rate;

The command is

[y,x] = sysode(2,1000,0,1000,[0,0,0]);

I arbitrarily chose these initial conditions. For this problem, it doesn't matter since the steady state is independent of the initial condition.



From the tabular output file,

9.9600000e+002 9.1309434e+003 1.4130943e+004 8.6905653e+002 9.9700000e+002 9.1309434e+003 1.4130943e+004 8.6905653e+002 9.9800000e+002 9.1309434e+003 1.4130943e+004 8.6905653e+002 9.9900000e+002 9.1309434e+003 1.4130943e+004 8.6905653e+002 1.0000000e+003 9.1309434e+003 1.4130943e+004 8.6905653e+002

we find that the steady state concentration of A is 9130.94, B is 14130.94 and C is 869.06  $mole/m^3$ .

We now perform the PFR analysis with the inlet stream given as the output of the CSTR.

The input file is

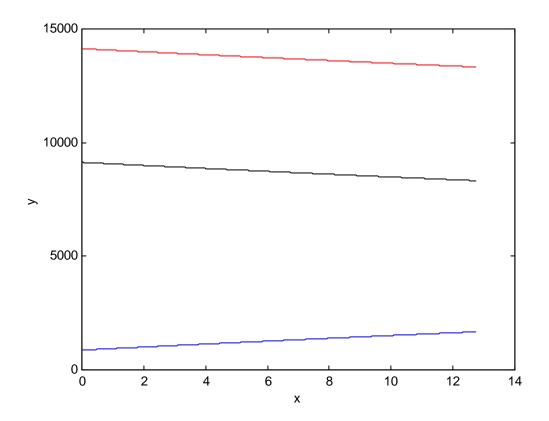
```
function dydt = sysodeinput(x,y,nvec);
%
% one reaction
% A + B --> C
%
% example usage:
% [y,x] = sysode(2,1000,0,12.7324,[9.1309434e+003, 1.4130943e+004, 8.6905653e+002]);
%
CA = y(1);
CB = y(2);
CC = y(3);
```

% nuA = -1.0;nuB = -1.0;nuC = 1.0;% % constant volume; F = 2.0; % liter/sec  $F = 2.0/1000; \% m^3/sec$ % % R = 8.314; % J/mol/KT = 300; % K ko = 1.0e-3; % liter/mol/sec  $ko = ko/1000; \% m^3/mol/sec$ Ea = 5000; % J/mol  $k = ko^{*}exp(-Ea/(R^{*}T));$ rate = k\*CA\*CB; % % circular pipe % Vtot = 100.0; % liters Vtot = Vtot/1000; % cubic meters Dp = 0.10; % mAcross = 0.25\*pi\*Dp\*Dp; % m^2 l = Vtot/Across; % m v = F/Across; % m/str = l/v; % sec % % molar balances % % dCAdz = nuA\*r/vdydt(1) = (nuA\*rate)/v;dydt(2) = (nuB\*rate)/v;dydt(3) = (nuC\*rate)/v;

The command is

[y,x] = sysode(2,1000,0,12.7324,[9.1309434e+003, 1.4130943e+004, 8.6905653e+002]);

I chose the length arbitrarily but the length and diameter must be chosen to maintain the proper total volume of the reactor.



From the tabular output file,

# 1.2732400e+001 8.3250921e+003 1.3325092e+004 1.6749079e+003

we find that the final steady state concentration of A leaving the reactor is  $8325 \text{ mole/m}^3$ .

The conversion of A

$$X_A = 1 - \frac{C_A}{C_{A,in}} = 1 - \frac{8325}{10000} = 0.1675$$

(b) What is the net conversion of A if the reactors are placed in series with the PFR first and CSTR second?

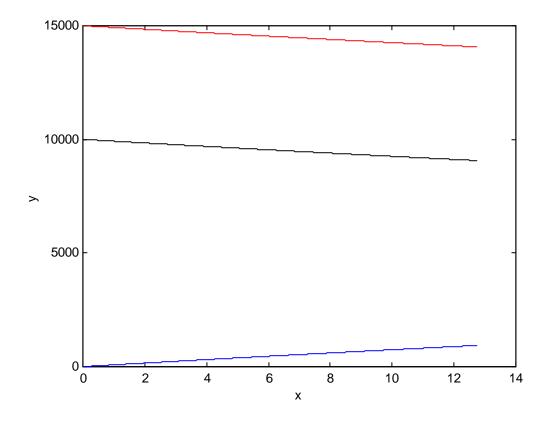
The input file for the PFR does not change.

The command is

[y,x] = sysode(2,1000,0,12.7324,[10000, 15000, 0]);

which provides the appropriate inlet concentrations.

# The output looks as follows



The last line of the output file is

```
1.2732400e+001 9.0682304e+003 1.4068230e+004 9.3176962e+002
```

from which we find that the steady state concentration leaving the PFRof A is 9068.23, B is 14068.23 and C is 931.77 mole/ $m^3$ .

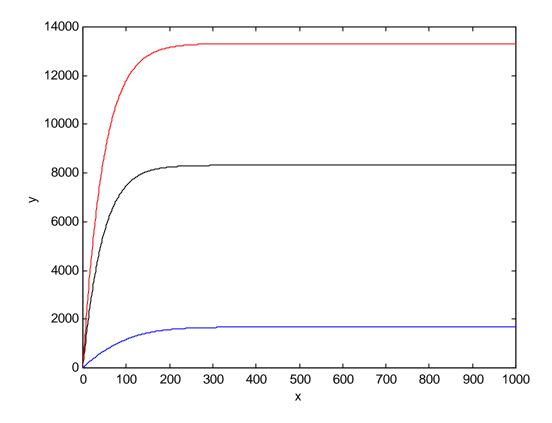
We now put this into the inlet concentration for the CSTR, which does require a change in the input file.

```
function dydt = sysodeinput(x,y,nvec);
%
% one reaction
% A + B --> C
%
% example usage:
% [y,x] = sysode(2,1000,0,1000,[0,0,0]);
%
CA = y(1);
CB = y(2);
CC = y(3);
%
nuA = -1.0;
```

nuB = -1.0;nuC = 1.0;% % constant volume; F = 2.0; % liter/sec F = 2.0/1000; % m^3/sec Fin = F;Fout = F: CAin = 9.0682304; % mol/liter CBin = 14.068230; % mol/liter CCin = 0.93176962; % mol/liter CAin = CAin\*1000; % mol/m^3 CBin = CBin\*1000; % mol/m^3 CCin = CCin\*1000; % mol/m^3 % V = 100; % liter V = 100/1000; % m^3 R = 8.314; % J/mol/KT = 300; % K ko = 1.0e-3; % liter/mol/sec ko = ko/1000; % m^3/mol/sec Ea = 5000; % J/mol k = ko\*exp(-Ea/(R\*T));rate = k\*CA\*CB; % % molar balances % dydt(1) = Fin/V\*CAin - Fout/V\*CA + nuA\*rate; dydt(2) = Fin/V\*CBin - Fout/V\*CB + nuB\*rate; dydt(3) = Fin/V\*CCin - Fout/V\*CC + nuC\*rate;

The command is

[y,x] = sysode(2,1000,0,1000,[0,0,0]);



From the output file

9.9500000e+002 8.3215718e+003 1.3321571e+004 1.6784282e+003 9.9600000e+002 8.3215718e+003 1.3321571e+004 1.6784282e+003 9.9700000e+002 8.3215718e+003 1.3321571e+004 1.6784282e+003 9.9800000e+002 8.3215718e+003 1.3321571e+004 1.6784282e+003 9.9900000e+002 8.3215718e+003 1.3321571e+004 1.6784282e+003 1.0000000e+003 8.3215718e+003 1.3321571e+004 1.6784282e+003

We find that the final steady state concentration of A leaving the reactor is  $8322 \text{ mole/m}^3$ .

The conversion of A

$$X_A = 1 - \frac{C_A}{C_{A,in}} = 1 - \frac{8322}{10000} = 0.1678$$

It's just about the same conversion.

### 2. Gas-Phase Batch Reactor

Consider the gas-phase reaction

$$A + B \rightarrow C$$

with elementary mechanism such that the rate is

$$r = kC_A C_B$$

where the rate constants are given by

$$k = k_o \exp\left(-\frac{E_a}{RT}\right)$$

The temperature is 500 K. The pressure is constant at 10 atm. The activation energy for the reaction is 5000 J/mol. The rate constant prefactor for the reaction is 0.001 m<sup>3</sup>/mol/s.. Consider a batch reactor of variable volume . The initial mole fraction of A is 0.6 and B is 0.4. The initial volume of the reactor is 10 m<sup>3</sup>.

(a) Generate a plot of the concentration of A, B and C as a function of time.

(b) What is the concentration of C after 100 sec?

(c) What is the conversion of A after 100 sec?

(d) What is the volume of the reactor after 100 sec?

#### Solution:

(a) Generate a plot of the concentration of A, B and C as a function of time.

#### The input file is

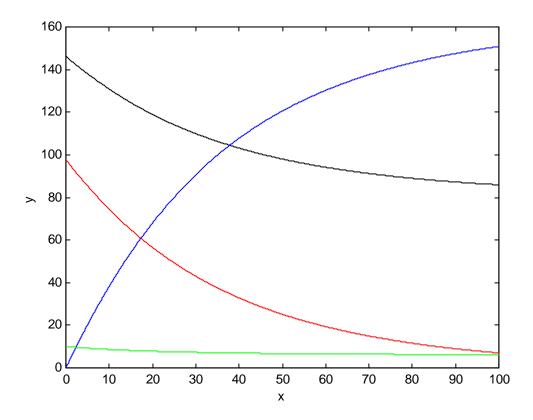
```
function dydt = sysodeinput(x,y,nvec);
% gas-phase batch reactor with variable volume
%
%
% sample usage:
% [y,x] = sysode(2,1000,0,2000,[146.2473,97.4982,0,10]);
% total initial concentration
%CTin = p/(R*T) = 243.7455 mol/m^3
% initial concentrations of A and B
%CAin = 0.6*CTin = 146.2473 mol/m^3
%CBin = 0.4*CTin = 97.4982 mol/m^3
%
CA = y(1);
CB = y(2);
CC = y(3);
V = y(4);
%
% A + B --> C
%
nuA = -1;
nuB = -1;
nuC = 1;
sumnu = nuA + nuB + nuC;
```

% % % p = 1013250.0; % Pa R = 8.314; % J/mol/K T = 500; % K%  $dVR = sumnu*R*T/p; \% m^3$ ko = 1.0e-3; % m^3/mol/sec Ea = 5000; % J/mol k = ko\*exp(-Ea/(R\*T));rate = k\*CA\*CB; % balance on A in terms of conc of A dydt(1) = (nuA - CA\*dVR)\*rate;% balance on B in terms of conc of B dydt(2) = (nuB - CB\*dVR)\*rate;% balance on C in terms of conc of C  $dydt(3) = (nuC - CC^*dVR)^*rate;$ % volume balance dydt(4) = dVR\*rate\*V;

The command is

[y,x] = sysode(2,1000,0,100,[146.2473,97.4982,0,10]);

where the initial concentrations are calculated using 60% and 40% of the total concentration at the given temperature and pressure, using the ideal gas law.



(b) What is the concentration of C after 100 sec?

From sysode.out, the values at 100 secs are

1.0000000e+002 8.5912877e+001 6.9965617e+000 1.5083607e+002 6.1773158e+000

So the concentration of C is  $150.83 \text{ moles/m}^3$ .

(c) What is the conversion of A after 100 sec?

The initial moles of A are

$$N_{A,in} = C_{A,in}V_{in} = 146.2473 \cdot 10 = 1462.473$$
 moles

The final number of moles is

$$N_{A,f} = C_{A,f}V_f = 85.91 \cdot 6.18 = 530.9$$
 moles

$$X_A = 1 - \frac{C_A}{C_{A,in}} = 1 - \frac{530.9}{1462.473} = 0.6370$$

(d) What is the volume of the reactor after 100 sec?

From the output, the final volume is  $6.18 \text{ m}^3$ .

### 3. Constant-Volume CSTRs with variable exit flowrate

Consider the gas-phase reaction

$$A + B \rightarrow C$$

with elementary mechanism such that the rate is

$$r = kC_A C_B$$

where the rate constants are given by

$$k = k_o \exp\left(-\frac{E_a}{RT}\right)$$

The temperature is 500 K and the pressure is 10 atm. The activation energy for the reaction is 5000 J/mol. The rate constant prefactor for the reaction is  $1.0 \text{ m}^3/\text{mol/s}$ . The feed flowrate is 1.0 m<sup>3</sup>/sec. The inlet feed stream is 60% A and 40% B.

(a) What is the steady state conversion of A?

(b) Provide a plot of the exit flow-rate as a function of time from your initial conditions to steady state.

(c) What is the steady state exit flow-rate?

#### Solution:

(a) What is the steady state conversion of A?

I used the following input file:

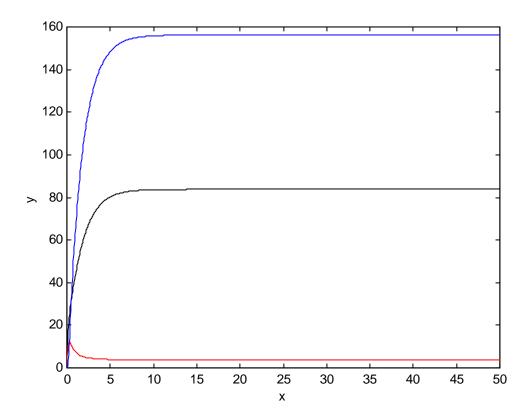
```
function dydt = sysodeinput(x,y,nvec);
%
% gas-phase CSTR with variable exit flow-rate
%
%
% sample usage:
% [y,x] = sysode(2,1000,0,100,[0,0,0]);
% initially tank is filled with A at one atm.
%
CA = y(1);
CB = y(2);
CC = y(3);
%
```

% A + B --> C% nuA = -1;nuB = -1;nuC = 1;sumnu = nuA + nuB + nuC;% % % p = 1013250.0; % Pa R = 8.314; % J/mol/KT = 500; % K  $CTin = p/(R*T); \% mol/m^3$ % initial concentrations of A and B CAin = 0.6\*CTin; % mol/m^3 CBin = 0.4\*CTin; % mol/m^3 CCin = 0.0;%  $dVR = sumnu*R*T/p; \% m^3$ ko = 1.0; % m^3/mol/sec Ea = 5000; % J/mol  $k = ko^*exp(-Ea/(R^*T));$ rate = k\*CA\*CB; % Fin = 1.0; %  $m^{3/sec}$ V = 1.0; % m^3; Fout = Fin + dVR\*rate\*V; % % molar balances % dydt(1) = Fin/V\*CAin - Fout/V\*CA + nuA\*rate; dydt(2) = Fin/V\*CBin - Fout/V\*CB + nuB\*rate; dydt(3) = Fin/V\*CCin - Fout/V\*CC + nuC\*rate;

I used the following command:

[y,x] = sysode(2,1000,0,50,[0,0,0]);

The output plot was



The last lines of the output file are:

4.9700000e+001 8.3770723e+001 3.7833393e+000 1.5619143e+002 4.9750000e+001 8.3770723e+001 3.7833393e+000 1.5619143e+002 4.9800000e+001 8.3770723e+001 3.7833393e+000 1.5619143e+002 4.9850000e+001 8.3770723e+001 3.7833393e+000 1.5619143e+002 4.9900000e+001 8.3770723e+001 3.7833393e+000 1.5619143e+002 4.9950000e+001 8.3770723e+001 3.7833393e+000 1.5619143e+002 5.0000000e+001 8.3770723e+001 3.7833393e+000 1.5619143e+002

The steady steady state concentration of A is  $83.77 \text{ moles/m}^3$ .

The steady state conversion is

$$X_A = 1 - \frac{C_A}{C_{A,in}} = 1 - \frac{83.77}{146.2473} = 0.4272$$

where I used the ideal gas law to determine CA,in.

$$C_{A,in} = \frac{N}{V} = \frac{p}{RT} = 146.2473 \frac{\text{mol}}{\text{m}^3}$$

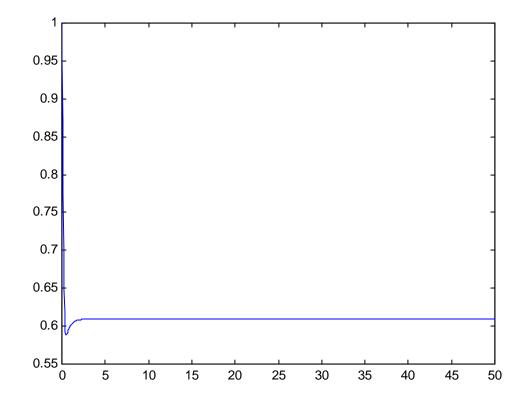
(b) Provide a plot of the exit flow-rate as a function of time from your initial conditions to steady state.

I typed the following commands in matlab

After I ran part A, I have the concentrations stored in the y matrix and time stored in the x vector.

I then ran

k = 0.30035; rate = k\*y(:,1).\*y(:,2); dVR = -0.00410264001974; Fin = 1.0; % m^3/sec V = 1.0; % m^3; Fout = Fin + dVR\*rate\*V; plot(x,Fout)



(c) What is the steady state exit flow-rate?

Fout(1001) =  $0.60945984012260 \text{ m}^3/\text{sec}$ The steady state outlet flowrate is  $0.61 \text{ m}^3/\text{sec}$ .